

## A358 Taunton to Southfields Dualling Scheme

Preliminary Environmental Information Report - Appendix 14.1 Greenhouse Gas Assessment Assumptions, Methodology and Emissions Factors

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## 1 Greenhouse gas (GHG) assessment assumptions, methodology and emissions factors

- 1.1 GHG emissions assessment supporting information
- 1.1.1 Table 1-1 of this appendix presents all assumptions made in the quantification of the capital carbon assessment, presented in Chapter 14 Climate of the Preliminary Environmental Information (PEI) Report.

 Table 1-1
 GHG assessment assumptions

| Item category | Location         | Description  | Quantity | Units                  | Assumptions   |
|---------------|------------------|--|----------|------------------------|---|
| Pavements     | Mainline         | Pavements - Surface course -<br>Close graded macadam - Thin -<br>in carriageway, hard shoulder<br>and hard strip | 12,971   | m³<br>(cubic<br>metre) | <ol> <li>Assume the density of close bitumen macadam is 1,700Kg/m³ (kilograms per cubic metre).</li> <li>Assume that close graded macadam has the same conversion factor as Asphalt.</li> <li>0.04m (metre) thickness = 22,050 tonnes.</li> </ol> |
| Pavements     | Mainline         | Pavements - Binder course -<br>Dense bitumen macadam<br>(DBM50) in carriageway hard<br>shoulder and hard strip   | 16,213   | m <sup>3</sup>         | <ol> <li>Assume the density of dense bitumen macadam is 1,700Kg/m³.</li> <li>Assume the dense bitumen macadam has the same conversion factor as Asphalt.</li> <li>0.05m thickness = 27,563 tonnes.</li> </ol>                                     |
| Pavements     | Mainline         | Pavements - Base - Dense<br>bitumen macadam (DBM50): In<br>carriageway hard shoulder and<br>hard strip           | 74,581   | m <sup>3</sup>         | <ol> <li>Assume the density of dense bitumen macadam is 1,700Kg/m³.</li> <li>Assume the dense bitumen macadam has the same conversion factor as Asphalt.</li> <li>0.23m thickness = 126,788 tonnes.</li> </ol>                                    |
| Pavements     | Mainline         | Pavements - Sub-base type 1 unbound mixture: in carriageway, hard shoulder and hard strip                        | 74,581   | m³                     | <ol> <li>Assume the subbase type 1 is equivalent to natural aggregate.</li> <li>Assume the density of subbase type 1 is 2,000Kg/m³.</li> <li>0.23m thickness = 149,163 tonnes.</li> </ol>   |
| Pavements     | Mainline         | Pavements - Capping layer -<br>unbound mixture: in<br>carriageway, hard shoulder and<br>hard strip               | 139,435  | m³                     | <ol> <li>Assume the capping layer is equivalent to natural aggregate.</li> <li>Assume the density of subbase type 1 is 2,000Kg/m³.</li> <li>0.43m thickness = 278,869 tonnes.</li> </ol>  |
| Pavements     | Mainline Overlay | Pavements - Surface course -<br>Close graded macadam - Thin -<br>in carriageway, hard shoulder<br>and hard strip | 3,072    | m³                     | <ol> <li>Assume the density of close bitumen macadam is 1,700Kg/m³.</li> <li>Assume that close graded macadam has the same conversion factor as Asphalt.</li> <li>0.04m thickness = 5,222 tonnes.</li> </ol>                                      |
| Pavements     | Mainline Overlay | Pavements - Binder course -<br>Dense bitumen macadam<br>(DBM50) in carriageway hard<br>shoulder and hard strip   | 3,839    | m <sup>3</sup>         | <ol> <li>Assume the density of dense bitumen macadam is 1,700Kg/m³.</li> <li>Assume the dense bitumen macadam has the same conversion factor as Asphalt.</li> <li>0.05m thickness = 6,527 tonnes.</li> </ol>                                      |
| Pavements     | Mainline Overlay | Pavements - Base - Dense bitumen macadam (DBM50): In   | 12,286   | m³                     | 1. Assume the density of dense bitumen macadam is 1,700Kg/m³. 2. Assume the dense bitumen macadam has the same conversion   |

| Item category | Location               | Description  | Quantity | Units          | Assumptions  |
|---------------|------------------------|--|----------|----------------|--|
|               |                        | carriageway hard shoulder and hard strip   |          |                | factor as Asphalt. 3. 0.16m thickness = 20,886 tonnes.   |
| Pavements     | Side roads and slips   | Pavements - Surface course - Close graded macadam - Thin - in carriageway, hard shoulder and hard strip        | 3,904    | m <sup>3</sup> | <ol> <li>Assume the density of close bitumen macadam is 1,700Kg/m³.</li> <li>Assume that close graded macadam has the same conversion factor as Asphalt.</li> <li>0.04m thickness = 6,637 tonnes.</li> </ol>   |
| Pavements     | Side roads and slips   | Pavements - Binder course -<br>Dense bitumen macadam<br>(DBM50) in carriageway hard<br>shoulder and hard strip | 4,880    | m³             | <ol> <li>Assume the density of dense bitumen macadam is 1,700Kg/m³.</li> <li>Assume the dense bitumen macadam has the same conversion factor as Asphalt.</li> <li>0.05m thickness = 8,296 tonnes.</li> </ol>   |
| Pavements     | Side roads and slips   | Pavements - Base - Dense bitumen macadam (DBM50): In carriageway hard shoulder and hard strip                  | 15,617   | m³             | <ol> <li>Assume the density of dense bitumen macadam is 1,700Kg/m³.</li> <li>Assume the dense bitumen macadam has the same conversion factor as Asphalt.</li> <li>0.16m thickness = 26,548 tonnes.</li> </ol>  |
| Pavements     | Side roads and slips   | Pavements - Sub-base type 1 unbound mixture: in carriageway, hard shoulder and hard strip                      | 24,401   | m³             | Assume the subbase type 1 is equivalent to natural aggregate.     Assume the density of subbase type 1 is 2,000Kg/m³.     0.25m thickness = 48,802 tonnes.   |
| Pavements     | Side roads and slips   | Pavements - Capping layer -<br>unbound mixture: in<br>carriageway, hard shoulder and<br>hard strip             | 41,482   | m <sup>3</sup> | Assume the capping layer is equivalent to natural aggregate.     Assume the density of subbase type 1 is 2,000Kg/m³.     0.425m thickness = 82,964 tonnes.   |
| Pavements     | Type 1 Access<br>Track | Pavements - Sub-base type 1 unbound mixture: in carriageway, hard shoulder and hard strip                      | 6,810    | m³             | <ol> <li>Assume the subbase type 1 is equivalent to natural aggregate.</li> <li>Assume the density of subbase type 1 is 2,000Kg/m³.</li> <li>0.23m thickness = 13,620 tonnes.</li> </ol>   |
| Pavements     | Type 1 Access<br>Track | Pavements - Capping layer -<br>unbound mixture: in<br>carriageway, hard shoulder and<br>hard strip             | 11,843   | m³             | <ol> <li>Assume the capping layer is equivalent to natural aggregate.</li> <li>Assume the density of subbase type 1 is 2,000 Kg/m³.</li> <li>0.4m thickness = 23,686 tonnes.</li> </ol>  |
| Barriers      | Central reserve        | Concrete step barrier  | 14,500   | m              | 1. Steel N2 has been specified within verges, where required. A rigid concrete step barrier (CSB) has been specified along the length of the proposed scheme within the majority of the central reserve. A working width for all barriers has been assumed to be |

| Item category | Location                  | Description  | Quantity | Units | Assumptions  |
|---------------|---------------------------|--|----------|-------|--|
|               |                           |  |          |       | W2. This will result in a steel post at 2m spacings. Transition and terminal lengths have been included within the total lengths for each option. A 0.4mx0.4mx0.6m concrete foundation would be required for 20% of VRS posts. The remaining would be driven posts.  2. Carbon conversion factor taken from the Highways England carbon tool. 1.2 tonnes per metre = 17,400 tonnes.  |
| Barriers      | Central reserve           | Steel barrier N2   | 13,653   | m     | 1. Steel N2 has been specified within verges, where required. A rigid concrete step barrier (CSB) has been specified along the length of the proposed scheme within the majority of the central reserve. A working width for all barriers has been assumed to be W2. This will result in a steel post at 2m spacings. Transition and terminal lengths have been included within the total lengths for each option. A 0.4mx0.4mx0.6m concrete foundation would be required for 20% of Vehicle Restraint Systems (VRS) posts. The remaining would be driven posts.  2. Carbon conversion factor taken from the Highways England carbon tool. 0.04 tonnes per metre = 485 tonnes. |
| Pavements     | Combined footway/cycleway | Pavements - Surface course -<br>Close graded macadam - Thin -<br>in carriageway, hard shoulder<br>and hard strip | 177      | m³    | <ol> <li>Assume the density of close bitumen macadam is 1,700Kg/m³.</li> <li>Assume that close graded macadam has the same conversion factor as Asphalt.</li> <li>0.02m thickness = 301 tonnes.</li> <li>Footways have been calculated from length of footpath multiplied by the average width of 3.5m. Splitter islands have been included on three of the arms (North, South, West) of the Nexus 25 roundabout. Build up based on light vehicle overrun specification in accordance with CD 239.</li> </ol>  |
| Pavements     | Combined footway/cycleway | Pavements - Binder course -<br>Dense bitumen macadam<br>(DBM50) in carriageway hard<br>shoulder and hard strip   | 443      | m³    | <ol> <li>Assume the density of dense bitumen macadam is 1,700Kg/m³.</li> <li>Assume the dense bitumen macadam has the same conversion factor as Asphalt.</li> <li>0.05m thickness = 753 tonnes.</li> <li>Footways have been calculated from length of footpath multiplied by the average width of 3.5m. Splitter islands have been included on three of the arms (North, South, West) of the Nexus 25 roundabout. Build up based on light vehicle overrun specification in accordance with CD 239.</li> </ol>  |

| Item category | Location                                      | Description  | Quantity | Units | Assumptions   |
|---------------|---|--|----------|-------|---|
| Pavements     | Combined footway/cycleway                     | Pavements - Sub-base type 1<br>unbound mixture: in<br>carriageway, hard shoulder and<br>hard strip | 1,994    | m³    | <ol> <li>Assume the subbase type 1 is equivalent to natural aggregate.</li> <li>Assume the density of subbase type 1 is 2,000Kg/m³</li> <li>0.225m thickness = 3,988 tonnes.</li> <li>Footways have been calculated from length of footpath multiplied by the average width of 3.5m. Splitter islands have been included on three of the arms (North, South, West) of the Nexus 25 roundabout. Build up based on light vehicle overrun specification in accordance with CD 239.</li> </ol>                    |
| Pavements     | Fencing                                       | Fencing - Timber post and rail   | 294,652  | m     | <ol> <li>Assume one access gate per access track and that existing fencing is degraded and needs replacement.</li> <li>Assume timber post and rail to be used for all fencing.</li> <li>Ecology mitigation will be required at numerous locations without the proposed scheme, e.g. otter proofing around watercourses, however this information is not available at present.</li> <li>Carbon conversion factor taken from the Highways England carbon tool. 0.01 tonnes per metre = 4,209 tonnes.</li> </ol> |
| Pavements     | Kerb lengths                                  | Pavements - Kerb lengths -<br>Edging   | 2,532    | m     | The back of the combined footway/cycleway is to use edging kerb. Kerbing has also been included at roundabouts and entries/exits. Kerbing has been included with the assumed splitter islands on the Nexus 25 roundabout.      Carbon conversion factor taken from the Highways England carbon tool. 0.09 tonnes per metre = 222 tonnes.  |
| Pavements     | Kerb lengths                                  | Pavements - Kerb lengths - HB2   | 3,032    | m     | The back of the combined footway/cycleway is to use edging kerb. Kerbing has also been included at roundabouts and entries/exits. Kerbing has been included with the assumed splitter islands on the Nexus 25 roundabout.      Carbon conversion factor taken from the Highways England carbon tool. 0.09 tonnes per metre = 266 tonnes.  |
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Pipe 150-300mm diameter - length (m)   | 31,600   | m     | Plastic, High-density polyethylene (HDPE).     Carbon conversion factor taken from the Highways England carbon tool. 0.97 tonnes per metre = 30,652 tonnes.   |
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Pipe 375-600mm diameter -<br>length (m)  | 12,150   | m     | Plastic, HDPE.     Carbon conversion factor taken from the Highways England carbon tool. 0.97 tonnes per metre = 11,786 tonnes.   |

| Item category | Location                                      | Description                                 | Quantity | Units           | Assumptions   |
|---------------|---|---|----------|-----------------|---|
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Pipe 675-900mm diameter - length (m)        | 700      | m               | Concrete.     Carbon conversion factor taken from the Highways England carbon tool. 0.89 tonnes per metre = 622 tonnes.   |
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Surface Water Channel - length (m)          | 27,350   | m               | <ol> <li>Concrete.</li> <li>Carbon conversion factor taken from the Highways England carbon tool. 0.15 tonnes per metre = 410 tonnes.</li> </ol>  |
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Linear Channel - length (m)                 | 450      | m               | Concrete.     Carbon conversion factor taken from the Highways England carbon tool. 0.15 tonnes per metre = 68 tonnes.  |
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Kerb Drain - length (m)                     | 780      | m               | Concrete, pre-cast.     Carbon conversion factor taken from the Highways England carbon tool. 0.09 tonnes per metre = 68 tonnes.  |
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Manhole Chamber 1200mm<br>diameter - number | 885      | no.<br>(number) | <ol> <li>Concrete, pre-cast.</li> <li>Carbon conversion factor taken from the Highways England carbon tool. 5.95 tonnes per metre = 5,266 tonnes.</li> </ol>  |
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Headwall - number                           | 250      | no.             | 1. Concrete, pre-cast. 2. Worst-case scenario was assumed from the selection of headwalls that accommodated 900mm (millimetre) diameter pipes. Link: https://www.althon.co.uk/products/h10c-f-headwall/detail/. 3. As per the assumption above, each headwall assumed to be 3.375 tonnes per unit = 844 tonnes total. 4. Emissions factor assumed to be the same as precast concrete. |
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Fill - Filter Drain - Volume (m3)           | 5,050    | m³              | Type 1 aggregate.     Carbon conversion factor taken from the Highways England carbon tool. 2.00 tonnes per metre = 10,100 tonnes.  |
| Drainage      | Mainline and<br>Local Roads<br>Sections 1 & 2 | Fill - Carrier Drain - Volume m3            | 33,600   | m <sup>3</sup>  | 1. If as-dug material is of good quality, this will be used for carrier drain bedding and fill. Assume material is of sufficient quality.  2. Carbon conversion factor taken from the Highways England carbon tool. 2.00 tonnes per metre = 67,200 tonnes.  |
| Earthworks    | Across proposed scheme                        | Fill material                               | 58,705   | m <sup>3</sup>  | Additional fill material required is assumed to be new material (natural aggregate).     Assume the density of fill material is 2,000Kg/m³ = 117,410 tonnes.  |

| Item category       | Location               | Description  | Quantity | Units | Assumptions  |
|---------------------|------------------------|--|----------|-------|--|
| Labour and<br>Plant | Across proposed scheme | Labour and plant emissions                               | n/a      | n/a   | 1. No information is available at this stage to calculate labour and plant for the proposed scheme. As such, an average has been calculated using the respective labour and plant footprints (normalised by km) of the schemes listed in Table 14-18 of Chapter 14 Climate of this PEI Report.   |
| Maintenance         | Across proposed scheme | Maintenance emissions                                    | n/a      | n/a   | No information is available at this stage to calculate maintenance for the proposed scheme. As such, an average has been calculated using the respective maintenance footprints (normalised by kilometre (km)) of the schemes listed in Table 14-18 of Chapter 14 Climate of this PEI Report.      Assume surface course is replaced once every 15 years and that pavements are replaced every 40 years. |
| Structures          | Across proposed scheme | Structures - Fill material                               | 36,156   | m³    | 1. Carbon conversion factor taken from the Highways England carbon tool. 2.00 tonnes per m <sup>3</sup> = 72,312 tonnes.   |
| Structures          | Across proposed scheme | Structures - In situ concrete                            | 7,658    | m³    | 1. Carbon conversion factor taken from the Highways England carbon tool. 2.4 tonnes per m <sup>3</sup> = 18,379 tonnes.  |
| Structures          | Across proposed scheme | Structures - Precast concrete                            | 6,628    | m³    | 1. Carbon conversion factor taken from the Highways England carbon tool. 2.4 tonnes per m <sup>3</sup> = 15,906 tonnes.  |
| Structures          | Across proposed scheme | Structures - Steel                                       | 377      | m³    | 1. Carbon conversion factor taken from the Highways England carbon tool. 8.00 tonnes per m <sup>3</sup> = 3,018 tonnes.  |
| Transport           | Across proposed scheme | Emissions from traffic during operation and construction | n/a      | n/a   | Assumptions are detailed in Tag traffic model.   |
| Water               | Across proposed scheme | Water use from operation                                 | n/a      | n/a   | Carbon emissions resulting from the consumption of water required by the proposed scheme to enable it to operate and deliver its service are assumed to be insignificant.  |